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Analysis and Control Systems for Shaft Vibration in Steel Rolling Processes

Katsuhiko Doi, Kozo Ishikawa, Hifumi Tsukuda, Kazuaki Yamamoto, Namio Suganuma, Tadashi Naito

Synopsis :

In recent years, the authors have been endeavoring to revamp steel rolling processes by realizing continuous and synchronized production between two processes in order to achieve higher quality of products. In cold and hot tandem mills or continuous annealing process lines, which required high response and high accuracy to the motor control system, the authors encountered troubles with shaft vibrations caused by interaction between mechanical and electrical control systems, and developed a new power drive technique which was effective in solving the problems. And authors were able to understand the influence of all the digital thyrister motor drive system and the cross current type cycloconverter drive system on the shaft vibration problem through computer simulation analyses and experiment



Analysis and Control Systems for Shaft Vibration in Steel Rolling Processes*







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of high strength material for mechanical structures has led to a decrease in shaft cross section, and a decrease in the mechanical torsion natural frequency N_f of equipment. The torque amplifying factor TAF at the resonant point has also been adversely affected.

(2) Flexural Bending Vibration in Mechanical Drive System

When flexure eccentricity or imbalance exists in



- the shaft system, the system vibrates at integermultiples of the rotary frequency of the roll- and motorshafts. If, because of higher operating speeds, $N_{\rm f}$ lies within the actual-use rotary frequency, thorough examination is indicated.
- (3) Vibration of Mechanical Structures and Foundation
- (4) Vibration of Strip Being Rolled

Clogging, slipping, changes in deformation charac-

- $\dot{\theta}$: Angular velocity (rpm)
- T_d : Torque disturbance (kgf·m)
- T_L : Load torque (kgf·m)
- R_s : Armature circuit resistance (Ω)
- F_{E} : Voltage coefficient (V/rpm)
- Fn: Speed feedback gain (mpm/rpm)
- $F_{\rm c}$: Current feedback gain
- S: Laplacian
- K_{T} : Torque coefficient

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$\begin{array}{c} 20 \\ (10) \\ (20)$	 Considering mechanical system as rigid body Considering mechanical system as one-degree-of-free 1 Tr ω₂ -40 dB/dec 	$\begin{array}{c} \hline f_1 \\ \hline Motor \\ \hline C_{12} \\ \hline K_{12}: \\ \hline C_{12} \\ \hline K_{12}: \\ \hline Equivalent torsional spring constant \\ \hline C_{12}: \\ \hline Equivalent damping coefficient \\ \hline Fig. 5 \\ \hline Mechanical resonance system \\ \hline \end{array}$
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	4.1.2 Simulation analysis comparison of analog control and digital control of thyristor Leonard control	$\left \begin{array}{c} y \\ x_4 \end{array} \right 2$ (0.77)	$\begin{vmatrix} y \\ x_4 \end{vmatrix} = \begin{pmatrix} 1.43 \\ (1.31) \\ (1.62) \end{vmatrix}$
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۲	 4.2 Effect of Speed Feedback Filter of Digital-type Thyristor Leonard Control System on Speed Response and Its Shaft Vibration Suppression Effect 4.2.1_Characteristics of speed feedback_filter 	80 60 40 60 20 5 5 5 5 60 60 60 60 60 60 60 60 60 60 60 60 60	$\begin{bmatrix} 0 \\ -30 \\ -60 \end{bmatrix}$
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