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Kawasaki Steel has tried to enhance the accuracy of microstructure control for developing various  $t$  pes of automotive ferrous materials having markedly improved properties, as well as to develop technologies for effectively using ferrous materials.

This paper outlines two e amples of newly commerciali ed automotive steel sheets. The rst is a new high strength hot rolled steel sheet that has e cellent strain age hardenabilit<sub>/</sub>, the tensile strength of which is increased by paint baking treatment (BHT steel sheet). The second is a highly formable high strength hot rolled steel sheet obtained by applying  $\ddot{d}$  namic recrystalli ation to re  $n$ ing cr<sub>/</sub>stal grains (Super HSLA steel sheet).

ing tensile strength of the materials. The new and conventional steel sheets show identical correlation between the absorbed energy and tensile strength when tested in the as-produced condition. When the were tested after giving 10% prestrain and paint baking treatment, the absorbed energ<sub>/</sub> showed a positive correlation with the tensile strength of each material. However, the absolute value of absorbed energ for the newl developed steel sheet is higher than that for the conventional steel sheet. The absorbed energ is increased b work hardening for both the conventional steel sheet and the newl developed steel sheet, but for the latter there is also the contribution of tensile strength increase due to strain age hardening. The contribution of strain age hardening is equivalent to the tensile strength increase of about 60 MPa in as-produced materials. The tensile strength increase (BHT) observable in normal tensile tests appears also in high strain rate tensile tests.

Based on the data obtained in this test, FEM anal/sis was carried out to evaluate the effect of the newl developed steel sheet on improving crashworthiness when used as a structural member of a vehicle. It was found that the contribution from the strain age hardening corresponds to a half-gauge (0.1 mm) increase in the sheet thickness and to a 60 to 70 MPa increase in tensile strength. Thus, it was con rmed that the newly developed steel sheet can make a vehicle signi cantl lighter as thinner gauge sheets can be used. It also helps make a vehicle lighter thanks to its e-cellent formability for various parts of comple shapes that are dif cult to form, thus reducing the strength of sheet required for such parts. $^{3)}$ 

Conventional steel sheets that have strain age hardenabilit<sub>/</sub> suffer deterioration of mechanical properties while held at room temperature. In contrast, the newl developed steel sheet held at room temperature for one year showed only negligible changes in properties: the tensile strength showed almost no change, the  $j$ ield strength increased  $b_1$  about 30 MPa, and the elongation lowered onl<sub> $/$ </sub> b<sub> $/$ </sub> 1%.

The newl developed steel sheet is produced  $b/$  controlling the chemical composition and grain si e of steel and is characterized by excellent strain age hardenability and less deterioration of properties  $\mathbf{b}_{j}$  room temperature aging.

The newl developed steel sheet allows crashworthiness to be improved without increasing vehicle weight, or conversely a vehicle to be made lighter while maintaining crashworthiness, and is e pected to make a signi cant contribution to safet $/$  and environmental issues associated with motor vehicles. It was alread reported that the use of this steel sheet for anti-collision members reduced the weight of a mass-produced vehicle by more than  $10\%$ .<sup>4)</sup> This steel sheet is e pected to be widel used in motor vehicles in the future.

## **3 Highly Formable High Strength Hot Rolled Steel Sheet Obtained by Applying Dynamic**

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tic. In other words, Ti does not cause much grain elongation, which deteriorates hole e pansion, even if the rolling temperature moves from the  $d$  namic recr stalli ation region to the static recrystalli ation region near the nal pass of hot rolling.

Steels having different Ti contents were e perimentally prepared, reheated to different temperatures, and compressed at 850°C, a temperature corresponding to the finish rolling temperature one in hot rolling. The relation between true stress and true strain was e amined in each case (**Fig. 5**). When a material undergoes d/namic recr/stalli/ation, its true stress-true strain curve e hibits a particular shape that has a peak. The stress increases with increasing strain until the strain reaches a certain strain level  $(\varepsilon_n)$ , where it shows the peak stress  $(\sigma_n)$ , then begins decreasing and becomes constant after the strain passes a certain value. These curves show that  $d$ <sub>/</sub> namic recr<sub>/</sub>stalli<sub>z</sub> ation tends to take place when the Ti content is high, and the reheating temperature is low. This is because the amount of TiC precipitation increases with decreasing compression temperature, and accordingl, the  $\gamma$  grain si e becomes smaller. In the case of low-carbon steel as in this test,  $d$  namic recr /stalli ation takes place even in the nish rolling region when the austenite grain si e is less than about 50  $\mu$ m.

The values of the peak stress obtained  $b/$  the compression test were plotted against the values of the parameter (**Fig. 6**), and used to calculate the apparent activation energy. The value obtained was 340 kJ/mol, which is near the self-diffusion activation energ  $\sigma$  of iron (285 kJ/mol). Thus,  $d/$ namic recr/stalli ation that takes place in these materials is interpreted with good consistenc  $\mu$  in terms of activation energ  $\mu$  as well.

The ferrite grain si es in the materials e perimentall compressed to the true strain of 0.7 and cooled at a rate of 50 $C/s$  were plotted as a function of reheating temperature (**Fig. 7**). The ferrite grain si es in the materials in which  $d/$  namic recr/stalliation took place (shown b/ solid ke<sub>/s</sub> in the gure) are markedl<sub>/</sub> smaller than those in the materials in which static recr/stalli ation took place. Thus, it was con rmed that a microstructure with ver  $\mu$  ne and uniform grain sizes of less than 5  $\mu$ m was obtained  $b/d$  namic recr stalligation.

## **3.2 Material Properties of the New Steel Sheet**

Currently, the Super HSLA steel sheets of 590 MPa class and 780 MPa class are being produced at Chiba Works. In both classes of steel sheets, it was con rmed that the aw stress is reduced  $b/10$  to 20% during nish rolling, and that  $d$  namic recr stalligation can be achieved in a commercial hot rolling process. **Photo 2** shows the microstructures of the newl developed Super HSLA steel sheet and conventional HSLA steel sheet. The average ferrite grain si e in the conventional steel sheet is 6 to 7  $\mu$ m, while that in the Super HSLA steel sheet is as ne as about  $2 \mu m$ . Thus, the compan, was the rst in the world to successfull produce, on an industrial scale, steel sheets that have ultra- ne grains.

The EBSD (electron back scattering diffraction) anal<sub>/</sub>sis of the microstructure of the newly developed steel sheet con rmed that the boundaries of adjacent grains have high angles of more than 15 . **Table 2** shows the mechanical properties of the newly developed steels of 590 MPa class and 780 MPa class. **Figure 8** compares the elongation and hole e pansion ratio of the newly developed steel sheet of 780 MPa class those of the conventional HSLA steel sheet. Both elongation and hole e pansion ratio are improved, whereas generall in the past, it was dif cult to improve these two properties